

# Optimal Design of Accelerated Life Tests with Multiple Stresses

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# Outline

- Motivation for ALT with multiple stresses
- Review current work on multiple stresses ALT
- Optimal Latin hypercube designs for ALT
- Modified simulated annealing algorithm
- Numerical examples
- Summary

# Motivation for ALT with Multiple Stresses

- Definition: *ALT is conducted to quickly obtain failure times in order to evaluate and predict reliability at normal operating conditions*
- Most of the previous work on designing ALT plans uses single stress
- For highly reliable products, it is difficult to obtain failures in a short time with single stress
- Reliability may depend on several stresses operating simultaneously.
- Multiple stresses represent realistic field conditions

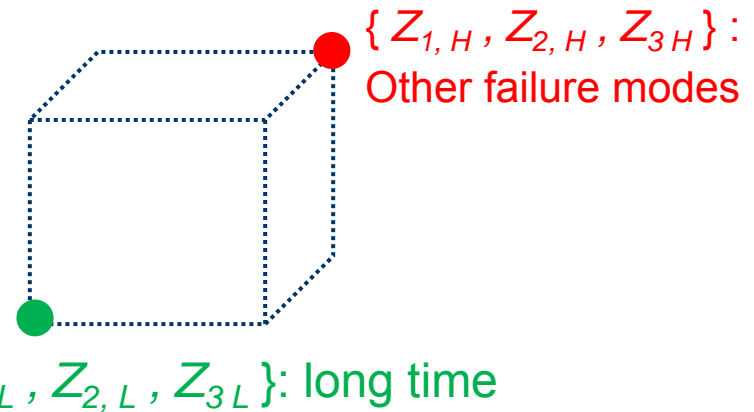
# Current Work on Multiple Stresses ALT

- Two stresses and two levels for each stress:
  - Nelson (1990) -- one accelerated stress and one other factor
  - Escobar and Meeker (1995) -- compromise plan
  - Park and Yum (1996) -- factorial design
  - Elsayed and Zhang (2009) -- factorial design
- Difficult to extend existing methods, because:
  - Multiple stresses and levels can result a huge number of stress-level combinations (designs).
  - With limited number of test units and time, how to choose the best or a small number of optimal designs?
  - How to spread the design points across the design region to avoid extreme conditions?

# Proposed Solution – Latin Hypercube Design

- Latin hypercube design ( $n, k$ ):
  - An *LHD* with  $k$  factors and  $n$  levels (design points).
  - Each factor has  $n$  levels taken values in  $\{1, 2, \dots, n\}$
  - Example, *LHD*(5, 3) :

Volt	Temp	Humidity
1	3	4
2	5	1
3	1	5
4	4	2
5	2	3



- Advantages:
  - Three or more factors and levels can be investigated
  - Optimal *LHD* can avoid extreme stress-level combinations
  - Significantly reduce the stress-level combinations:  $n^k$  to  $n$ .

# Optimal *LHD* Criterion

- Inter-site distance:  $d(\mathbf{s}, \mathbf{t}) = \left\{ \sum_{j=1}^k |s_j - t_j|^q \right\}^{1/q}$

$q=1, 2, \infty$ , correspond to rectangular, Euclidean, and infinite distance

- Example:

$$\begin{array}{l}
 \begin{array}{|c|c|c|} \hline 1 & 3 & 4 \\ \hline 2 & 5 & 1 \\ \hline 3 & 1 & 5 \\ \hline 4 & 4 & 2 \\ \hline 5 & 2 & 3 \\ \hline \end{array} \longrightarrow \mathbf{s} \\
 LHD(n, k): \quad \begin{array}{|c|c|c|} \hline 2 & 5 & 1 \\ \hline 3 & 1 & 5 \\ \hline 4 & 4 & 2 \\ \hline 5 & 2 & 3 \\ \hline \end{array} \longrightarrow \mathbf{t} \\
 LHD(5, 3): \quad \begin{array}{|c|c|c|} \hline 4 & 4 & 2 \\ \hline 5 & 2 & 3 \\ \hline \end{array}
 \end{array}
 \quad \binom{n}{2} = \binom{5}{2} = 10 \text{ pairs of inter-site distance}$$

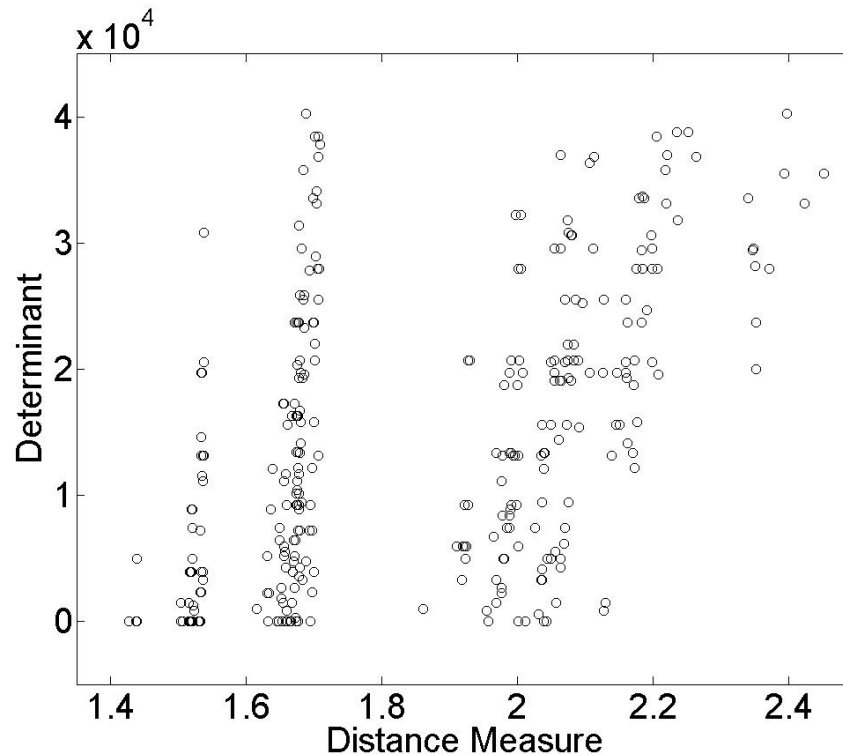
- Morris and Mitchell (1995) proposed maximum minimum inter-site distance criterion:

$$\phi_p = \left( \sum_{i=1}^{\binom{n}{2}} \frac{1}{d_i^p} \right)^{1/p}$$

- Spread the design points across the design region

# Optimal ALT Criterion

- *D*-optimality:
  - Ensure the accuracy of parameter estimation
  - Maximize determinant of Fisher information matrix of maximum likelihood estimate
- *D*-optimality may not lead to optimal distance measure



# Objective Function

- A multi-objective formulation:

$$\text{Min } -w \frac{\det(F_s(\mathbf{X}))}{\text{Det}_U} - (1-w) \frac{\Phi_{\rho}(\mathbf{X}) - \Phi_{\rho,L}}{\Phi_{\rho,U} - \Phi_{\rho,L}}, \quad w \in [0,1]$$

- $w$  is the weight
- $\mathbf{X}$  is the design matrix
- $\det(F_s(\mathbf{X}))$  is the determinant of the Fisher information matrix
- $\Phi_{\rho} = 1/\phi_{\rho}$  is the distance measure
- Normalize the distance and  $D$ -optimality criteria:
  - $\text{Det}_U$  is the upper bound of the determinant
  - $\Phi_{\rho,U}$  and  $\Phi_{\rho,L}$  are the upper and lower bound of the distance measure

# Propositions

- Focus on three stresses
  - Concurrently applying too many stresses is very demanding for test equipment
  - Extension to more stresses is possible

- For a  $LHD(n,3)$ ,  $0 \leq \det(F_s) \leq Det_U$

$$Det_U = n^4 (n-1)^3 (n+1)^3 (n\pi^2 + 2n\gamma(1-\gamma)) / 10368, n > 1$$

- For a  $LHD(n,k)$ ,  $\Phi_{p,L} \leq \Phi_p \leq \Phi_{p,U}$ ,  $q, p \in [1, \infty)$

$$\Phi_{p,U} = \left[ \sqrt{kn(n+1)/6} / \binom{n}{2}^{1/p} \right] \quad \Phi_{p,L} = \left( \sum_{i=1}^{n-1} \frac{(n-i)}{k^{p/2} \cdot i^p} \right)^{(-1/p)}$$

Proofs are given in our working paper

# Log-location Scale Model

- Log times to failure  $Y = \ln(T)$  is assumed to follow

$$f_Y = (y; \mu(\boldsymbol{\beta}\mathbf{x}), \sigma) = \frac{1}{\sigma} \exp\left[\left(\frac{y - \mu(\boldsymbol{\beta}\mathbf{x})}{\sigma}\right) - \exp\left(\frac{y - \mu(\boldsymbol{\beta}\mathbf{x})}{\sigma}\right)\right] \quad -\infty < y < \infty$$

- The location parameter depends on the stresses through

$$\mu(\boldsymbol{\beta}\mathbf{x}) = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \cdots + \beta_k x_k$$

- Transformation  $Y = \mu(\boldsymbol{\beta}\mathbf{x}) + \sigma Z$
- Extreme value distribution  $f_Z(z) = \exp(z - \exp(z))$ ,  $-\infty < z < \infty$
- Log likelihood function of failures observed in the  $m^{\text{th}}$  run

$$l_m = \ln L_m(\beta_0, \dots, \beta_k, \sigma) = -N\pi_m \ln(\sigma) + \sum_{j=1}^{(N\pi_m)} z_{m,j} - \sum_{j=1}^{(N\pi_m)} \exp(z_{m,j})$$

# Fisher Information Matrix

- Assume equal proportion of test units for each design point

$$F = N\pi_1 \sum_j F_{1,j} + N\pi_2 \sum_j F_{2,j} + \dots + N\pi_n \sum_j F_{n,j}$$

$$F = \frac{N}{n\sigma^2} \begin{bmatrix} n & \sum_{m=1}^n x_{1,m} & \dots & \dots & \sum_{m=1}^n x_{k,m} & n(1-\gamma) \\ \sum_{m=1}^n x_{1,m} & \sum_{m=1}^n x_{1,m}^2 & \sum_{m=1}^n x_{1,m}x_{2,m} & \dots & \sum_{m=1}^n x_{1,m}x_{k,m} & (1-\gamma) \sum_{m=1}^n x_{1,m} \\ \vdots & \vdots & \ddots & \vdots & \vdots & \vdots \\ \sum_{m=1}^n x_{k,m} & \sum_{m=1}^n x_{1,m}x_{k,m} & & & \sum_{m=1}^n x_{k,m}^2 & (1-\gamma) \sum_{m=1}^n x_{k,m} \\ n(1-\gamma) & (1-\gamma) \sum_{m=1}^n x_{1,m} & \dots & \dots & (1-\gamma) \sum_{m=1}^n x_{k,m} & n \left[ \frac{\pi^2}{6} + (\gamma - 1)^2 \right] \end{bmatrix}$$

where  $\gamma = 0.5777215$  is Euler's constant.

# Generation of *LHD*

- For the distance measure  $\phi_p$ , Morris and Mitchell (1995) used simulated annealing (SA) to generate *LHDs*:
  - Begin with a random chosen *LHD*
  - Perturb the current design  $D$  by interchanging two **randomly** chosen elements within a **randomly** chosen column of the design matrix
  - If the perturbed matrix  $D_{try}$  leads to an improvement, it is adopted as the new current design from which the next perturbation is generated
  - Otherwise, a replacement is made with probability

$$\pi = \exp\left\{-\left[\phi(D_{try}) - \phi(D)\right]/t\right\}$$

where  $t$  is the annealing temperature

- The algorithm stops either after given iterations or a tolerance criterion is met

# Modified SA to Generate *LHD* for ALT

- Choose the elements to interchange based on **probabilities**

- $LHD(n,3):$ 

$$\begin{bmatrix} 1 & x_{2,1} & x_{3,1} \\ 2 & \vdots & \vdots \\ \vdots & & \\ n & x_{2,n} & x_{3,n} \end{bmatrix}$$

- Maximum determinant of the Fisher information matrix is obtained

when  $a_1 = \sum_{m=1}^n x_{1,m} x_{2,m} = n(n+1)^2/4$  and  $a_2 = \sum_{m=1}^n x_{1,m} x_{3,m} = n(n+1)^2/4$

- Choose column based on probability

$$\left| a_1 - n(n+1)^2/4 \right|^p / \sum_{i=1,2} \left| a_i - n(n+1)^2/4 \right|^p, p \in [1, \infty)$$

- Choose row based on probability  $\Phi_{p,i}^p / \sum_{i=1}^n \Phi_{p,i}^p$  (Joseph and Hung, 2008 proposed  $\phi_{p,i}^p / \sum_{i=1}^n \phi_{p,i}^p$ )

# Numerical Example 1 – *LHD* (5,3)

- Testing stress levels for each factor:

<i>LHD</i>	1	2	3	4	5
Volts/cm <sup>2</sup>	12	16	20	24	28
Temperature (°C)	-40	0	40	80	120
Relative Humidity(RH)	20	30	40	50	60

- Set  $w = 0.5$

$(p,q)$	(5,1)					(5,2)						
	<i>LHD</i>			Volts/cm <sup>2</sup>	°C	RH	<i>LHD</i>			Volts/cm <sup>2</sup>	°C	RH
Complete enumeration & Modified SA	1	4	2	12	80	30	1	4	2	12	80	30
	2	3	5	16	40	60	2	1	3	16	-40	40
	3	2	1	20	0	20	3	5	4	20	120	50
	4	1	4	24	-40	50	4	2	5	24	0	60
	5	5	3	28	120	40	5	3	1	28	40	20

# Numerical Example 1 – Simulation

- Given parameter values:

$$\boldsymbol{\beta} = [423 \quad -12.6 \quad 6.2 \quad -3.7] \quad \sigma = 0.94$$

- Stress settings: optimal design from  $(p, q) = (5, 2)$
- Generate random failure times:

$$F_z = 1 - \exp(-\exp(z)) \quad z = \frac{\ln(t_i) - (\beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_3)}{\sigma}$$

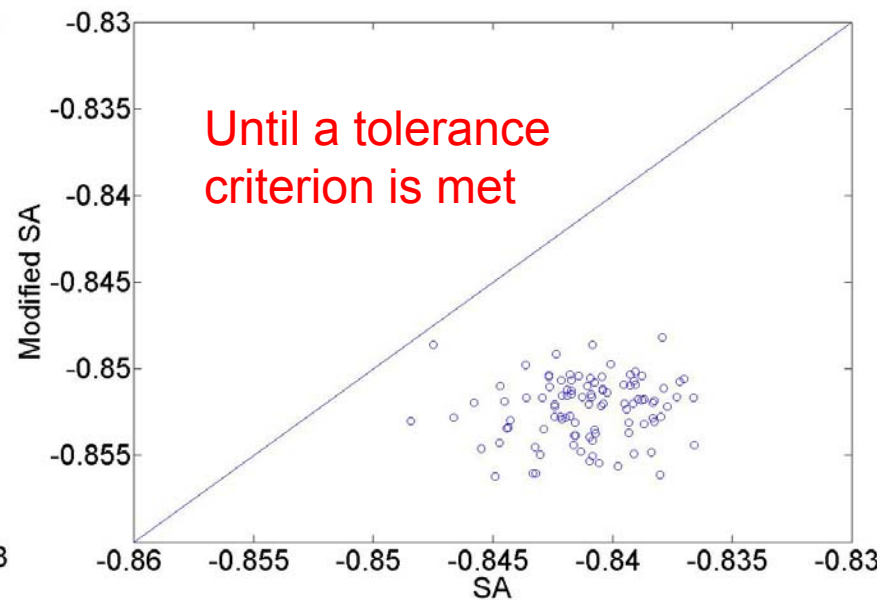
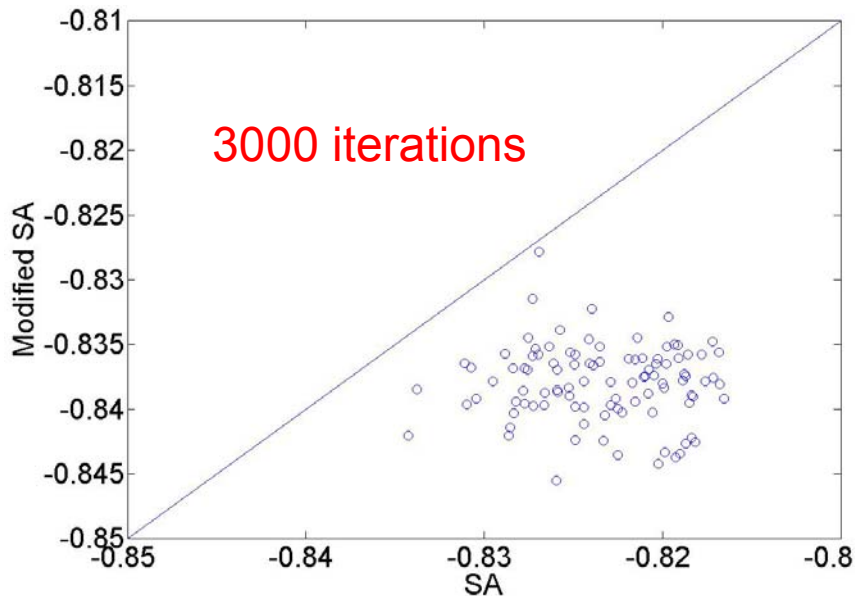
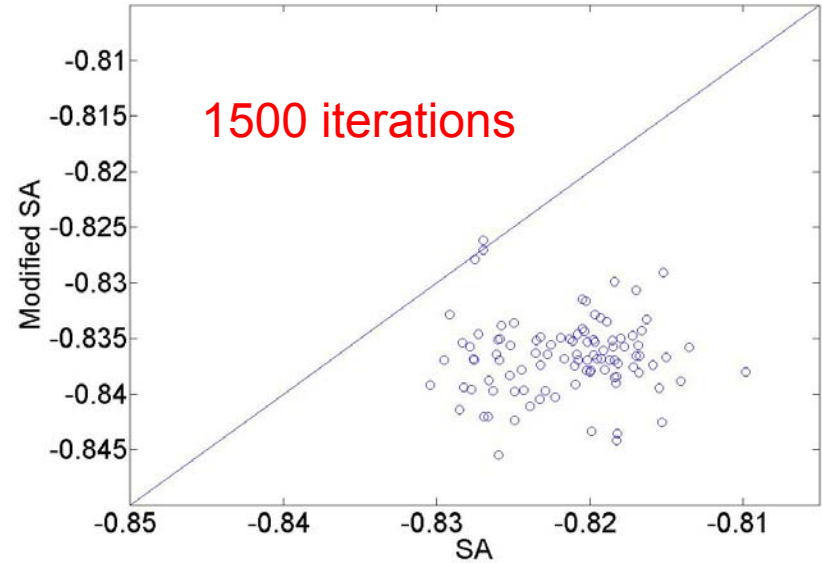
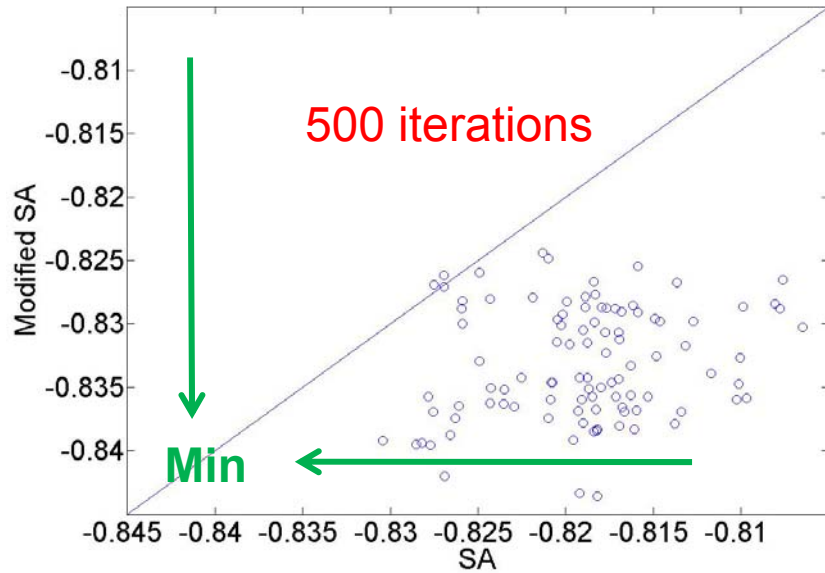
$$t_i = \exp\left[(\beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 x_3) + \sigma \ln[-\ln(1 - \text{rand}(i))]\right]$$

- Maximum likelihood estimate (repeat 100 times):

$$\hat{\boldsymbol{\beta}} = [422.9 \quad -12.6 \quad 6.19 \quad -3.69] \quad \hat{\sigma} = 0.91$$

$$\hat{\boldsymbol{\sigma}}_{\boldsymbol{\beta}} = [0.66 \quad -0.02 \quad 0.2 \quad -0.006] \quad \hat{\sigma}_{\hat{\sigma}} = 0.08$$

# Numerical Example 2 – *LHD* (25, 3)



# Numerical Example 2 – 300 Times Simulation

- Count smaller objective function values from MSA than those from SA

Stop Criterion	<i>LHD (10, 3)</i>		<i>LHD (25, 3)</i>	
	<i>q = 1</i>	<i>q = 2</i>	<i>q = 1</i>	<i>q = 2</i>
500 iter.	85.1%	90.2%	98%	95%
1500 iter.	88.3%	91%	98.5%	96.7%
3000 iter.	92%	92.5%	99.33%	98%
Tolerance	100%	100%	100%	100%

- Compare MSA and SA in terms of objective function values

<i>LHD (10,3)</i>	Min		Max		Mean	
<i>(p, q) = (15, 2)</i>	MSA	SA	MSA	SA	MSA	SA
500 iter.	<b>-0.8843</b>	-0.8741	<b>-0.8493</b>	-0.8273	<b>-0.8673</b>	-0.8529
1500 iter.	<b>-0.8891</b>	-0.8794	<b>-0.8557</b>	-0.8375	<b>-0.8731</b>	-0.8606
3000 iter.	<b>-0.8950</b>	-0.8825	<b>-0.8654</b>	-0.8484	<b>-0.8756</b>	-0.8657
tolerance	<b>-0.8918</b>	-0.8833	<b>-0.8756</b>	-0.8633	<b>-0.8821</b>	-0.8746

<i>LHD (25,3)</i>	Min		Max		Mean	
<i>(p, q) = (15, 2)</i>	MSA	SA	MSA	SA	MSA	SA
500 iter.	<b>-0.8500</b>	-0.8412	<b>-0.8298</b>	-0.8100	<b>-0.8395</b>	-0.8261
1500 iter.	<b>-0.8500</b>	-0.8423	<b>-0.8355</b>	-0.8112	<b>-0.8424</b>	-0.8287
3000 iter.	<b>-0.8519</b>	-0.8437	<b>-0.8360</b>	-0.8245	<b>-0.8433</b>	-0.8318
tolerance	<b>-0.8525</b>	-0.8473	<b>-0.8437</b>	-0.8338	<b>-0.8486</b>	-0.8386

# Summary

- Multiple stresses ALT plan is developed using Latin hypercube design, such that the stress-level combinations are dramatically reduced
- The  $D$ -optimality and maximin distance measures are normalized and combined to generate desired  $LHD$  for ALT
- Simulated annealing algorithm is modified to efficiently generate optimal  $LHD$ s.
- Numerical examples validate the feasibility and efficiency of the proposed methodology